

## **Project NF-CZ07-MOP-3-202-2015**

# **Frequency methods for solving nonlinear systems**

## Fourier series

$f(x)$  periodic function with period  $2\pi$  ...  $f(x + 2\pi) = f(x)$

$$f(x) = \frac{b_0}{2} + \sum_{n=1}^{\infty} (a_n \sin nx + b_n \cos nx)$$

$$a_n = \frac{1}{\pi} \int_{-\pi}^{\pi} f(x) \sin nxdx \quad \dots \quad n = 1, 2, 3, \dots$$

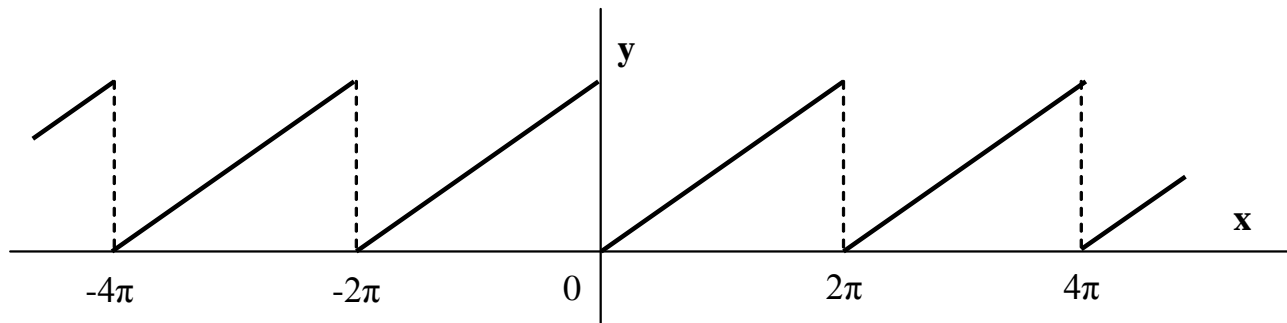
$$b_n = \frac{1}{\pi} \int_{-\pi}^{\pi} f(x) \cos nxdx \quad \dots \quad n = 0, 1, 2, \dots$$

base interval is arbitrary interval  $\langle a, a + 2\pi \rangle$

(not only  $\langle -\pi, \pi \rangle$  but also often  $\langle 0, 2\pi \rangle$  ... then  $\int_0^{2\pi} \dots$  )

**Example:** Let function  $f(x)$  is periodic with period  $2\pi$  and let it is in base interval  $\langle 0, 2\pi \rangle$  is given by equation  $f(x) = x$ .

Transform it to Fourier series.



$$a_n = \frac{1}{\pi} \int_0^{2\pi} x \sin nx dx = -\frac{1}{\pi} \left[ x \frac{\cos nx}{n} \right]_0^{2\pi} + \frac{1}{n\pi} \int_0^{2\pi} \cos nx dx = -\frac{2}{n} \quad \dots \quad n = 1, 2, 3, \dots$$

$$b_0 = \frac{1}{\pi} \int_0^{2\pi} x dx = 2\pi$$

$$b_n = \frac{1}{\pi} \int_0^{2\pi} x \cos nx dx = -\frac{1}{\pi} \left[ x \frac{\sin nx}{n} \right]_0^{2\pi} - \frac{1}{n\pi} \int_0^{2\pi} \sin nx dx = 0 \quad \dots \quad n = 1, 2, 3, \dots$$

**Result**

$$f(x) = \pi - 2 \left( \frac{\sin x}{1} + \frac{\sin 2x}{2} + \frac{\sin 3x}{3} + \dots \right)$$

**Periodic function with period 2l**

$$f(x) = \frac{b_0}{2} + \sum_{n=1}^{\infty} \left( a_n \sin \frac{n\pi x}{l} + b_n \cos \frac{n\pi x}{l} \right)$$

$$a_n = \frac{1}{l} \int_{-l}^l f(x) \sin \frac{n\pi x}{l} dx \quad \dots \quad n = 1, 2, 3, \dots \quad b_n = \frac{1}{l} \int_{-l}^l f(x) \cos \frac{n\pi x}{l} dx \quad \dots \quad n = 0, 1, 2, \dots$$

**Periodic functions with period T**

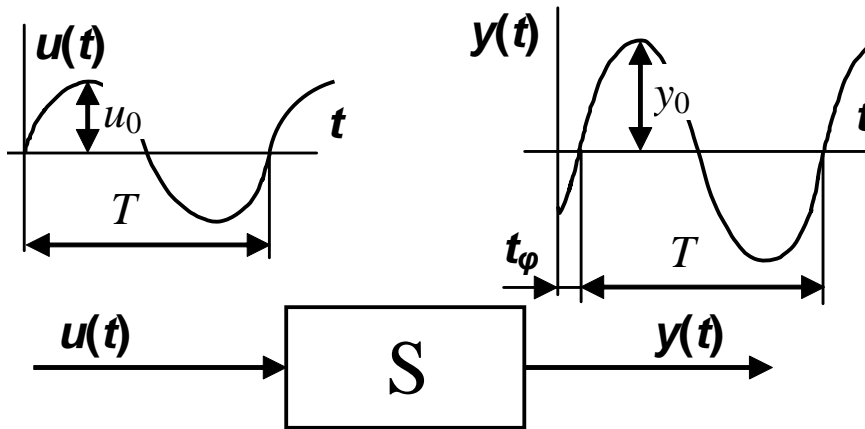
$$t \rightarrow x \quad \frac{\pi}{l} = \frac{\pi}{T/2} = \frac{2\pi}{T} = \omega \quad \omega \rightarrow \frac{\pi}{l}$$

$$f(t) = \frac{b_0}{2} + \sum_{n=1}^{\infty} (a_n \sin n\omega t + b_n \cos n\omega t)$$

$$a_n = \frac{2}{T} \int_0^T f(t) \sin n\omega t dt \quad \dots \quad n = 1, 2, 3, \dots \quad b_n = \frac{2}{T} \int_0^T f(t) \cos n\omega t dt \quad \dots \quad n = 0, 1, 2, \dots$$

**Equivalent transform**

Linear systems



$$u(t) = u_0 \sin \omega t$$

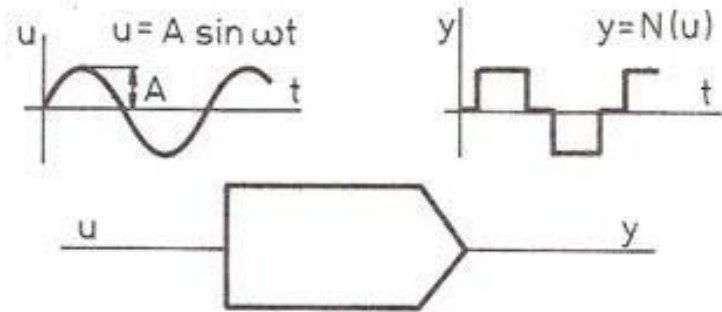
$$y(t) = y_0 \sin(\omega t + \varphi)$$

$$\mathbf{u}(t) = u_0 e^{j\omega t}$$

$$\mathbf{y}(t) = y_0 e^{j(\omega t + \varphi)}$$

$$G(j\omega) = \frac{\mathbf{y}(t)}{\mathbf{u}(t)} = \frac{y_0 e^{j(\omega t + \varphi)}}{u_0 e^{j\omega t}} = \frac{y_0}{u_0} e^{j\varphi}$$

**Nonlinear systems – brief summary**

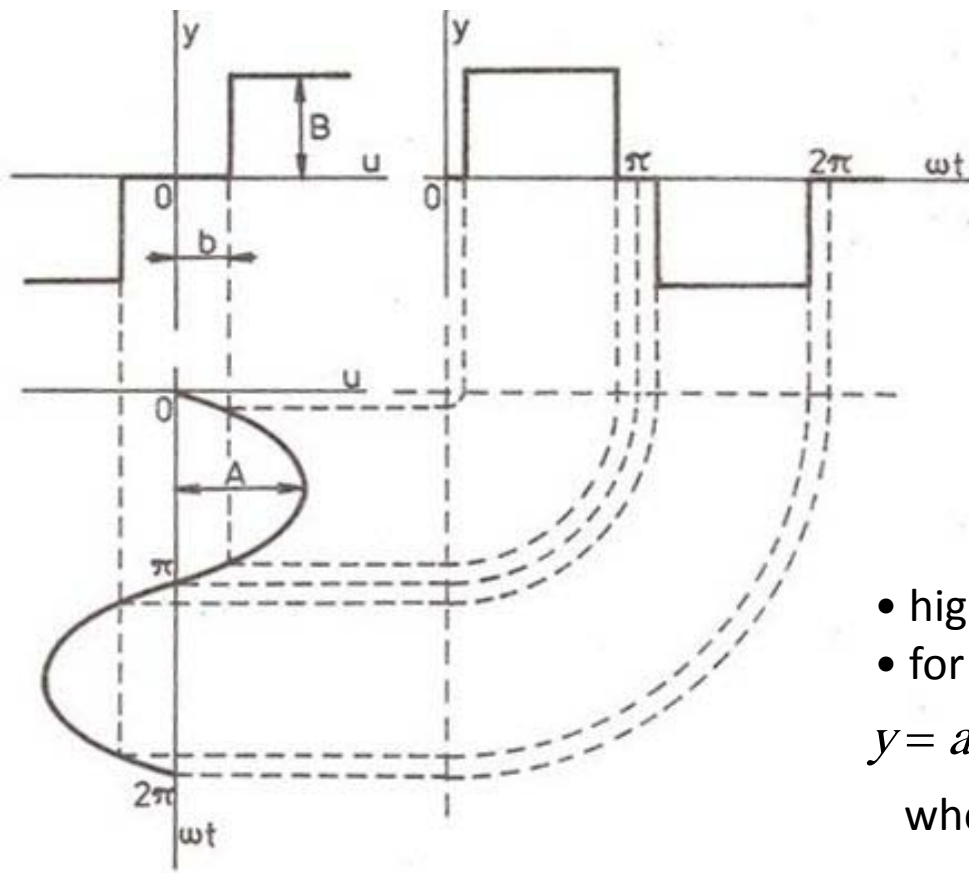


$$G_N(A) = \frac{\text{first harmonics of output}}{\text{sinusoidal input signal}} = \frac{Y}{U}$$

$$G_N(A) = a(A) + jb(A)$$

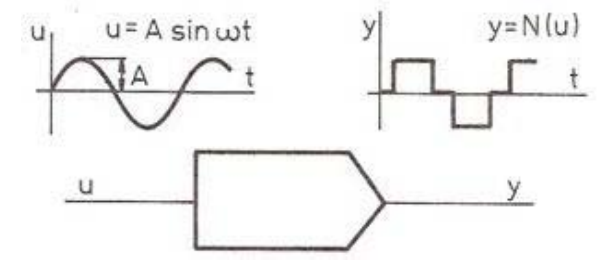
$a(A), b(A)$  coefficients of Fourier series for first harmonics

$b(A)$  proportional to surface of static characteristics – for explicit nonlinearity = 0



$$u = A \sin \omega t$$

$$y = N(u)$$



$$y = a_1 \sin \omega t + a_2 \sin \omega t + \dots$$

$$+ \frac{b_0}{2} + b_1 \cos \omega t + b_2 \cos \omega t + \dots$$

- higher harmonics filtered by linear parts
- for even functions is  $b_0 = 0$

$$y = a_1 \sin \omega t + b_1 \cos \omega t = Aa \sin \omega t + Ab \cos \omega t$$

where  $a_1 = Aa$  ;  $b_1 = Ab$

$$a_1 = \frac{2}{T} \int_0^T y(t) \sin n\omega t dt$$

$$a = \frac{a_1}{A} = \frac{2}{TA} \int_0^T y(t) \sin n\omega t dt = \frac{\omega}{\pi A} \int_0^T y(t) \sin n\omega t dt$$

$$b_1 = \frac{2}{T} \int_0^T y(t) \cos n\omega t dt$$

$$b = \frac{b_1}{A} = \frac{2}{TA} \int_0^T y(t) \cos n\omega t dt = \frac{\omega}{\pi A} \int_0^T y(t) \cos n\omega t dt$$



Transforming  $y$  to function only using sinus:  $a = c \cos \varphi$   $b = c \sin \varphi$

$$c^2 = a^2 + b^2 \quad ; \quad \operatorname{tg} \varphi = \frac{b}{a}$$

$$y = A(a \sin \omega t + b \cos \omega t) = A[c \cos \varphi \sin \omega t + c \sin \varphi \cos \omega t] = A c \sin(\omega t + \varphi)$$

Equivalent transfer – definition:  $G_N(A) = \frac{\text{first harmonics of output}}{\text{sinusoidal input signal}} = \frac{Y}{U}$

$$G_N(A) = \frac{Y}{U} = \frac{A c e^{j(\omega t + \varphi)}}{A e^{j\omega t}} = c e^{j\varphi} = c(\cos \varphi + j \sin \varphi) = a(A) + j b(A)$$

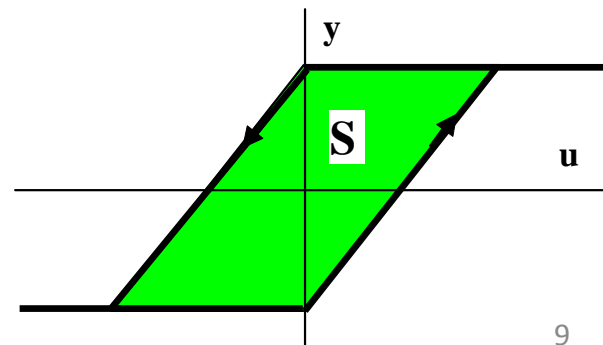
$G_N(A)$  is independent on frequency  $\omega$ , it is only function of input amplitude  $A$  !

**Important:**

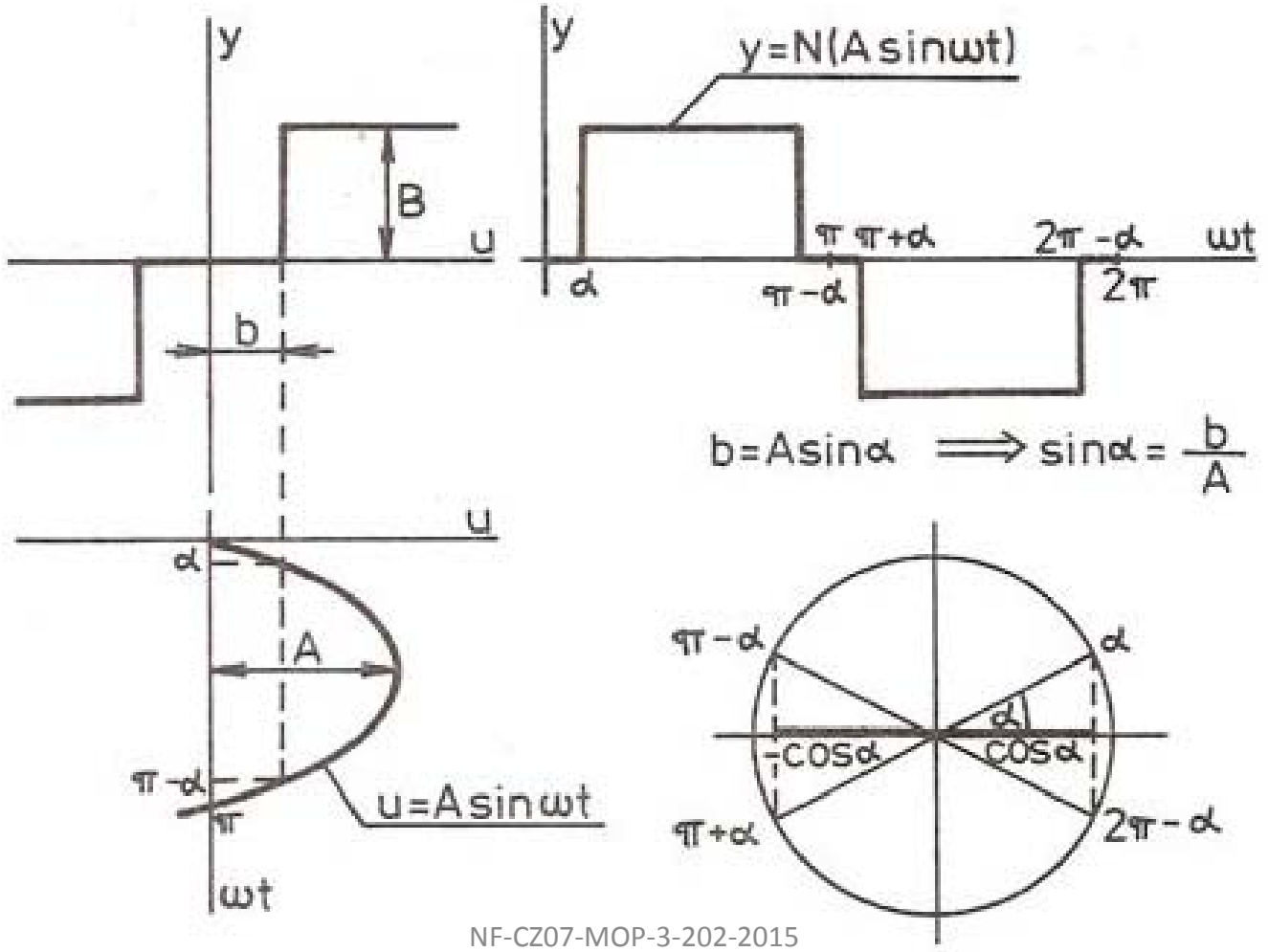
Imaginary part  $b(A)$  is proportional to area of static characteristics of nonlinear member. For terms with ambiguous nonlinearity:

$$b(A) \approx S$$

$$S = 0 \quad \rightarrow \quad G_N(A) = a(A)$$



**Example:** Determine equivalent transfer of nonlinear control member given by statistical characteristic of relay type with insensitivity band (given values  $b$ ,  $B$ ) by figure.



Solution:

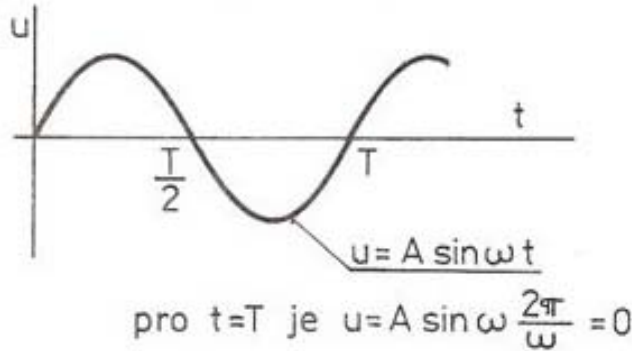
$$\begin{aligned}
 G_N(A) &= a(A) = \frac{\omega}{\pi A} \int_0^T y(t) \sin \omega t dt = \\
 &= \frac{\omega}{\pi A} \left[ \int_0^{\frac{\alpha}{\omega}} 0 \cdot \sin \omega t dt + \int_{\frac{\alpha}{\omega}}^{\frac{\pi-\alpha}{\omega}} B \cdot \sin \omega t dt + \int_{\frac{\pi-\alpha}{\omega}}^{\frac{\pi+\alpha}{\omega}} 0 \cdot \sin \omega t dt + \int_{\frac{\pi+\alpha}{\omega}}^{\frac{2\pi-\alpha}{\omega}} (-B) \cdot \sin \omega t dt + \int_{\frac{2\pi-\alpha}{\omega}}^{2\pi} 0 \cdot \sin \omega t dt \right] = \\
 &= \frac{\omega}{\pi A} \left[ \int_{\frac{\alpha}{\omega}}^{\frac{\pi-\alpha}{\omega}} B \cdot \sin \omega t dt - \int_{\frac{\pi+\alpha}{\omega}}^{\frac{2\pi-\alpha}{\omega}} B \cdot \sin \omega t dt \right] = \frac{\omega B}{\pi A} \left[ \left[ -\frac{1}{\omega} \cos \omega t \right]_{\frac{\alpha}{\omega}}^{\frac{\pi-\alpha}{\omega}} - \left[ -\frac{1}{\omega} \cos \omega t \right]_{\frac{\pi+\alpha}{\omega}}^{\frac{2\pi-\alpha}{\omega}} \right] = \\
 &= \frac{B}{\pi A} \left[ \left[ -\cos \omega t \right]_{\frac{\alpha}{\omega}}^{\frac{\pi-\alpha}{\omega}} + \left[ \cos \omega t \right]_{\frac{\pi+\alpha}{\omega}}^{\frac{2\pi-\alpha}{\omega}} \right] = \frac{B}{\pi A} \left( \left[ \cos \alpha + \cos \alpha \right] + \left[ \cos \alpha + \cos \alpha \right] \right) = \frac{4B}{\pi A} \cos \alpha
 \end{aligned}$$

$$\cos \alpha = \sqrt{1 - \sin^2 \alpha}$$

$$G_N(A) = \frac{4B}{\pi A} \sqrt{1 - \frac{b^2}{A^2}}$$

Has been used (figure)

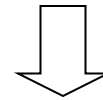
$$\cos(\pi - \alpha) = -\cos \alpha \quad ; \quad \cos(\pi + \alpha) = -\cos \alpha \quad ; \quad \cos(2\pi - \alpha) = \cos \alpha$$



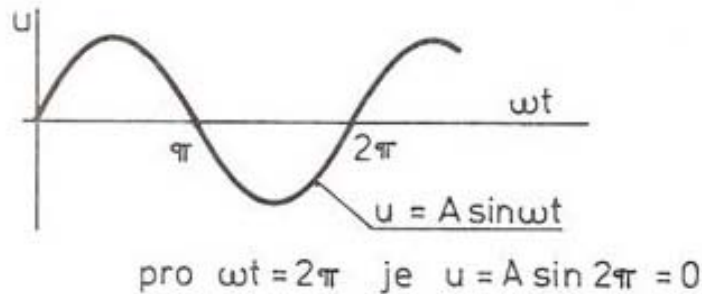
Is angle  $\alpha$  unknown – undefined?

$$u = A \sin \omega t$$

$$\text{for } \omega t = \alpha \text{ is } u = b \rightarrow b = A \sin \alpha$$



$$\alpha = \arcsin \frac{b}{A}$$



$$G_N(A) = \frac{\omega}{\pi A} \int_0^T y(t) \sin \omega t dt$$

It is more appropriate to have  $\omega t$  instead of  $t$  on horizontal axis.

$$G_N(A) = \frac{\omega}{\pi A_0} \int_0^T y(t) \sin \omega t dt \quad \langle \alpha, \pi - \alpha \rangle$$

It is integrated for whole period  $T$ . Period is divided to segments with constant  $y(t)$ . Output is  $\omega t$  and therefore are intervals  $\langle 0, \alpha \rangle, \langle \alpha, \pi - \alpha \rangle, \langle \pi - \alpha, \pi + \alpha \rangle$  etc. Corresponding angle must be divided by  $\omega$ . After integration we get terms like:

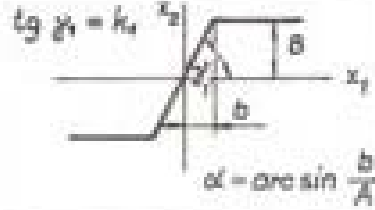
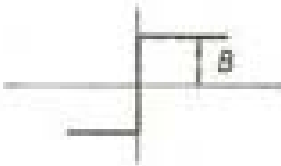
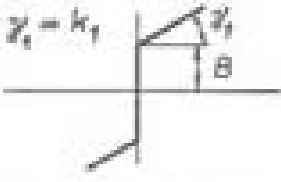
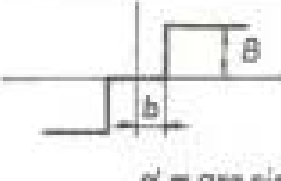
$$\left[ \cos \omega t \right]_{\frac{\alpha}{\omega}}^{\frac{\pi - \alpha}{\omega}}$$

and during assignment of limits, the  $\omega$  is eliminated.

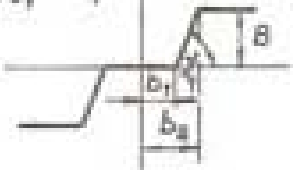

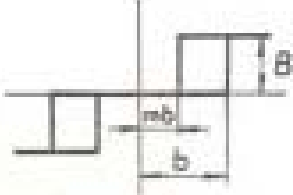
Equivalent transfers are in the table.

Ekvivalentní přenosy

Tab. 1.1

|  |   |
|--|---|
|  <p><math>\text{tg } \gamma_1 = k_1</math></p> <p><math>\alpha = \arcsin \frac{b}{A}</math></p> | $\sigma(A) = \frac{k_1}{\pi} (2\alpha - \sin 2\alpha) + \frac{4B}{\pi A} \cos \alpha$ |
|   | $\sigma(A) = \frac{4B}{\pi A}$  |
|  <p><math>\text{tg } \gamma_1 = k_1</math></p>   | $\sigma(A) = k_1 + \frac{4B}{\pi A}$  |
|  <p><math>\alpha = \arcsin \frac{b}{A}</math></p>   | $\sigma(A) = \frac{4B}{\pi A} \cos \alpha$  |

Equivalent transfers are in the table.

|   |   |
|---|---|
| <p><math>\operatorname{tg} \gamma_1 = k_1</math></p>  <p><math>\alpha_1 = \arcsin \frac{b_1}{A}</math><br/><math>\alpha_2 = \arcsin \frac{b_2}{A}</math></p> | $\sigma(A) = \frac{k_1}{\pi A} \left[ 2A(-\alpha_1 + \alpha_2) + A(\sin 2\alpha_1 - \sin 2\alpha_2) + 4b_1(\cos \alpha_2 - \cos \alpha_1) + \frac{4B}{\pi A} \cos \alpha_2 \right]$ |
| <p><math>\operatorname{tg} \gamma_1 = k_1</math></p>  <p><math>\alpha = \arcsin \frac{b}{A}</math></p>   | $\sigma(A) = \frac{k_1}{\pi A} \left[ A(\pi - 2\alpha) + A \sin 2\alpha - 4b \cos \alpha \right]$   |
|  <p><math>\alpha_1 = \arcsin \frac{b}{A}</math><br/><math>\alpha_2 = \arcsin \frac{mb}{A}</math></p>  | $\sigma(A) = \frac{2B}{\pi A} (\cos \alpha_1 + \cos \alpha_2)$ $b(A) = -\frac{2B}{\pi A} (\sin \alpha_1 - \sin \alpha_2)$   |

## Computation and display of equivalent transfers

**Example:** Nonlinear member is denoted by equation of its static characteristics

$$y = u^3$$

Compute it's equivalent transfer and amplitude characteristics in complex plane.

**Solution:** Input sinusoidal signal  $u = A \sin \omega t \rightarrow$  output signal

$$y = A^3 \sin^3 \omega t = \frac{A^3}{4} (3 \sin \omega t - \sin 3\omega t)$$

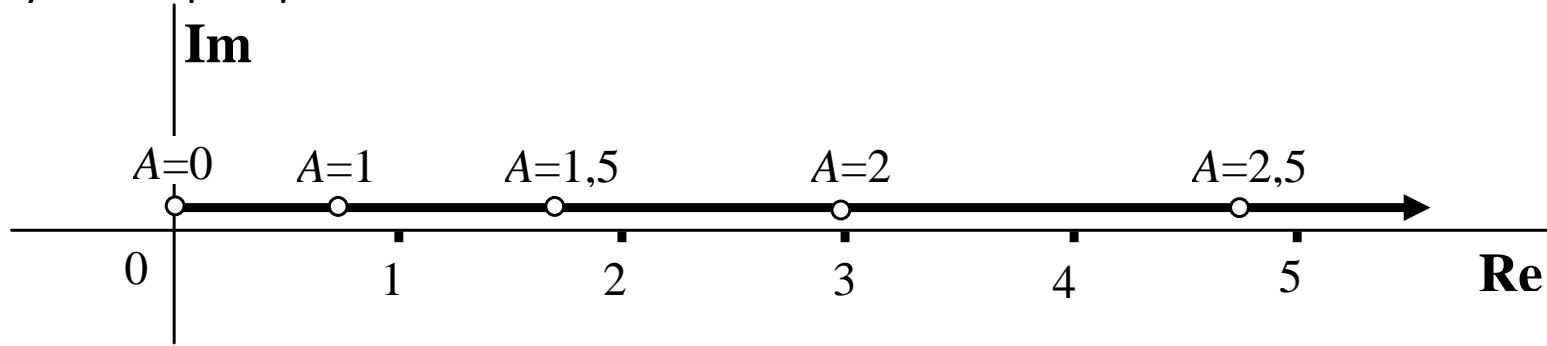
Use goniometric formula  $\sin^3 \alpha = \frac{1}{4} (3 \sin \alpha - \sin 3\alpha)$

Let's ignore third harmonics – definition of equivalent transfer in complex plane

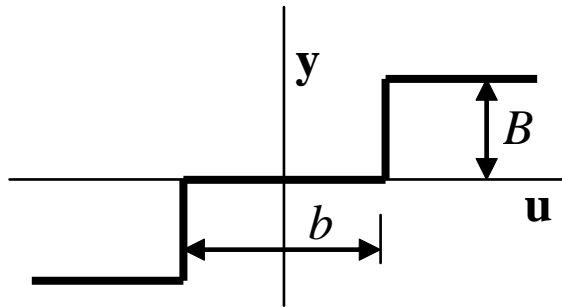
$$G_N(A) = \frac{\text{first hramonics of input}}{\text{sinusoidal output signal}} = \frac{A^3 \frac{3}{4} \sin \omega t}{A \sin \omega t} = \frac{3}{4} A^3$$



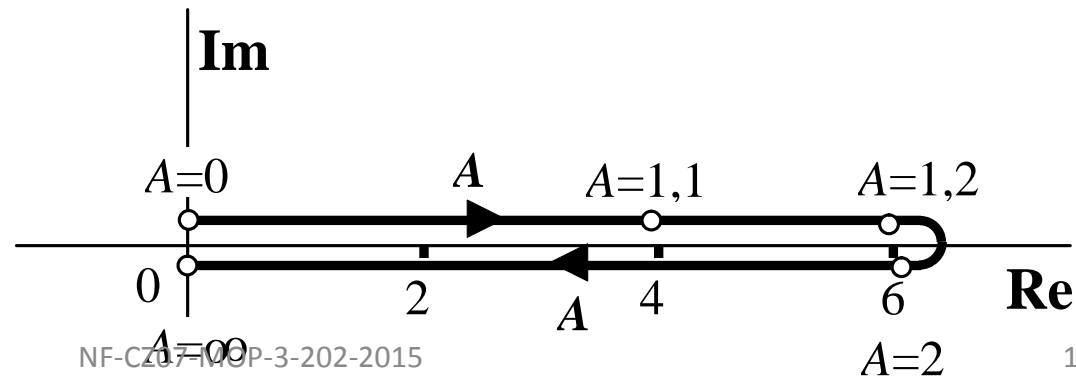
Display in complex plane



Relay with insensitivity band

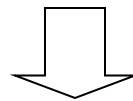


$$G_N(A) = \frac{4B}{\pi A} \sqrt{1 - \frac{b^2}{A^2}}$$

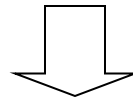


## Determining autooscillations in nonlinear circuits

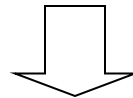
Autooscillation (stable limit cycle)



oscillations with constant amplitude

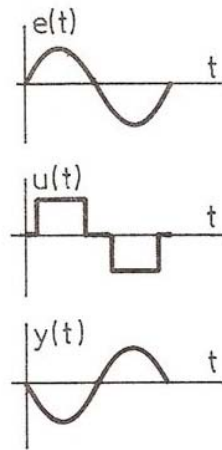
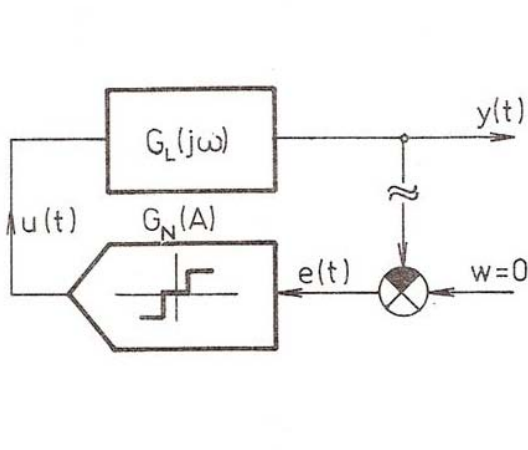


determine amplitude and frequency



avoid their creation

**Existence of autooscillations → output  $y(t)$  with phase shift to input by  $180^\circ$  but same amplitude.**



$$G_L(j\omega)G_N(A) = -1$$

common form

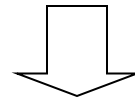
$$G_L(j\omega)G_N(A) + 1 = 0$$

Solution of this equation :  $A, \omega$  (if the autooscillations exist).

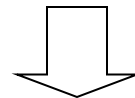
**Analytic solution:**  $\text{Re} [G_L(j\omega)G_N(A) + 1] = 0$

$$\text{Im} [G_L(j\omega)G_N(A) + 1] = 0$$

two equations for two variables  $A, \omega$

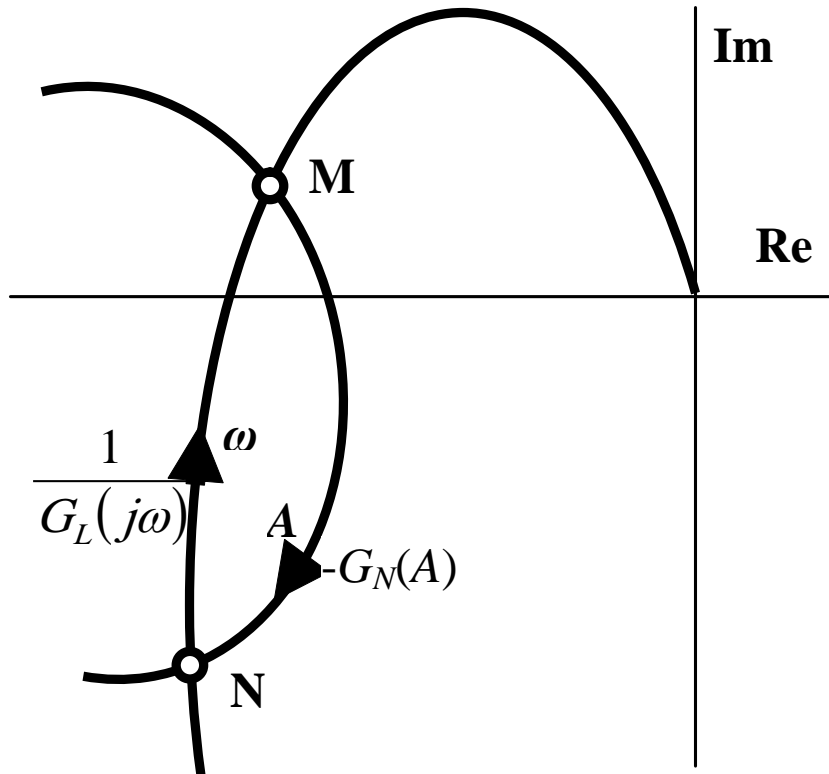


real solution



autooscillations exist and have computed parameters

Graphic solution :



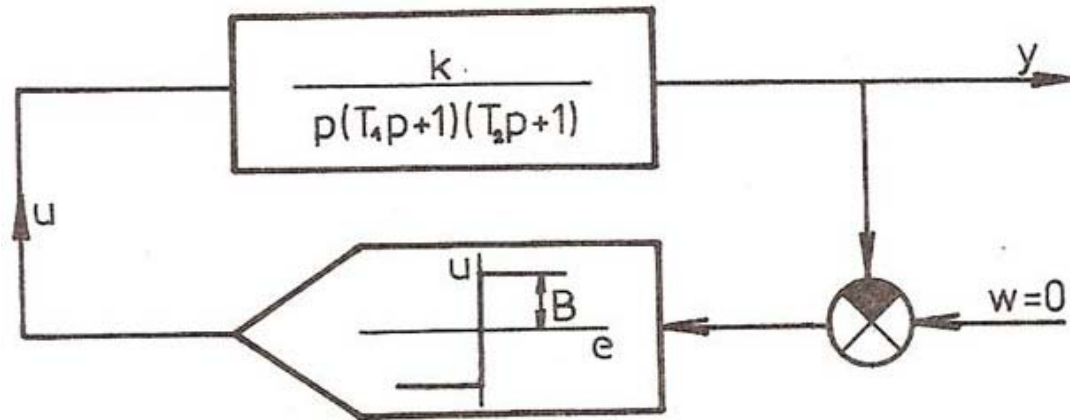
$$G_L(j\omega) = -\frac{1}{G_N(A)}$$

$$-G_L(j\omega) = \frac{1}{G_N(A)}$$

$$\frac{1}{G_L(j\omega)} = -G_N(A)$$

Intersections M , N  
? exist – not exist ?

**Example:** Nonlinear control circuit in figure consists of linear proportional system



( $k = 1$ ;  $T_1 = 1$ ;  $T_2 = 1$ ) with ideal two-value controller ( $B=1$ ). Determine if in the circuit emerge autooscillations and if they do determine amplitude and frequency.

Solve analytically and graphically.

**Solution:**  
Analytic:

$$G_N(A) = \frac{4B}{\pi A} \sqrt{1 - \frac{b^2}{A^2}} \quad \rightarrow \quad b = 0 \quad G_N(A) = \frac{4B}{\pi A}$$

$$G_L(j\omega)G_N(A) + 1 = 0 \quad \rightarrow \quad \frac{k}{j\omega(T_1 j\omega + 1)(T_2 j\omega + 1)} \cdot \frac{4B}{\pi A} + 1 = 0$$

$$k \frac{4B}{\pi A} - (T_1 + T_2)\omega^2 + j\omega(1 - T_1 T_2 \omega^2) = 0$$

Re = 0:  $k \frac{4B}{\pi A} - (T_1 + T_2)\omega^2 = 0$

Im = 0:  $\omega(1 - T_1 T_2 \omega^2) = 0$

Solution exists, autooscillations emerge. Amplitude and frequency:

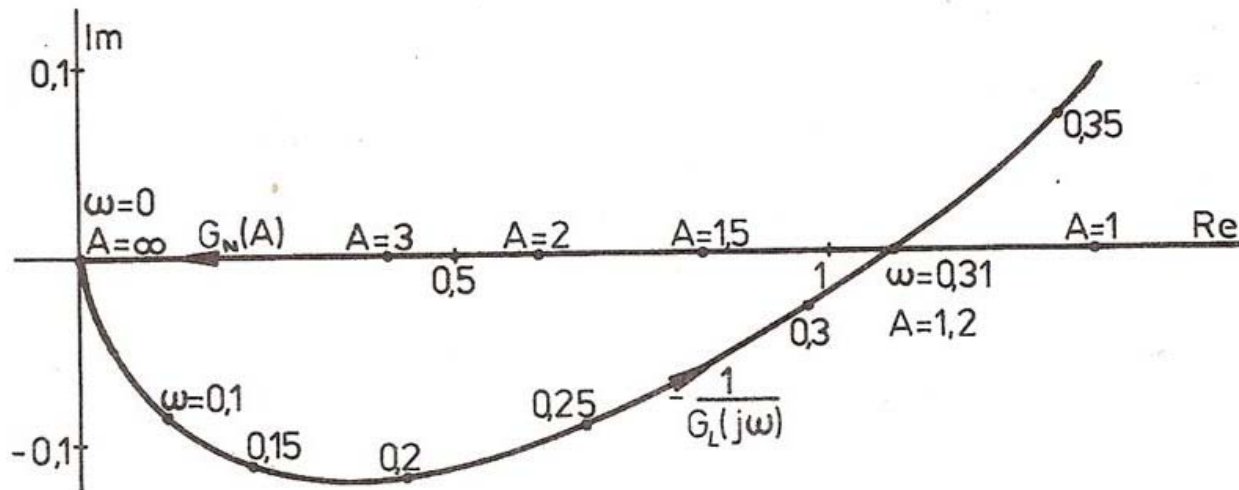
$$\omega = \sqrt{\frac{1}{T_1 T_2}} = \sqrt{\frac{1}{1.10}} = 0,316$$

$$A = \frac{T_1 T_2}{T_1 + T_2} \cdot \frac{4Bk}{\pi} = \frac{1.10}{1 + 10} \cdot \frac{4 \cdot 1.1}{\pi} = 1,1575$$

Graphic:

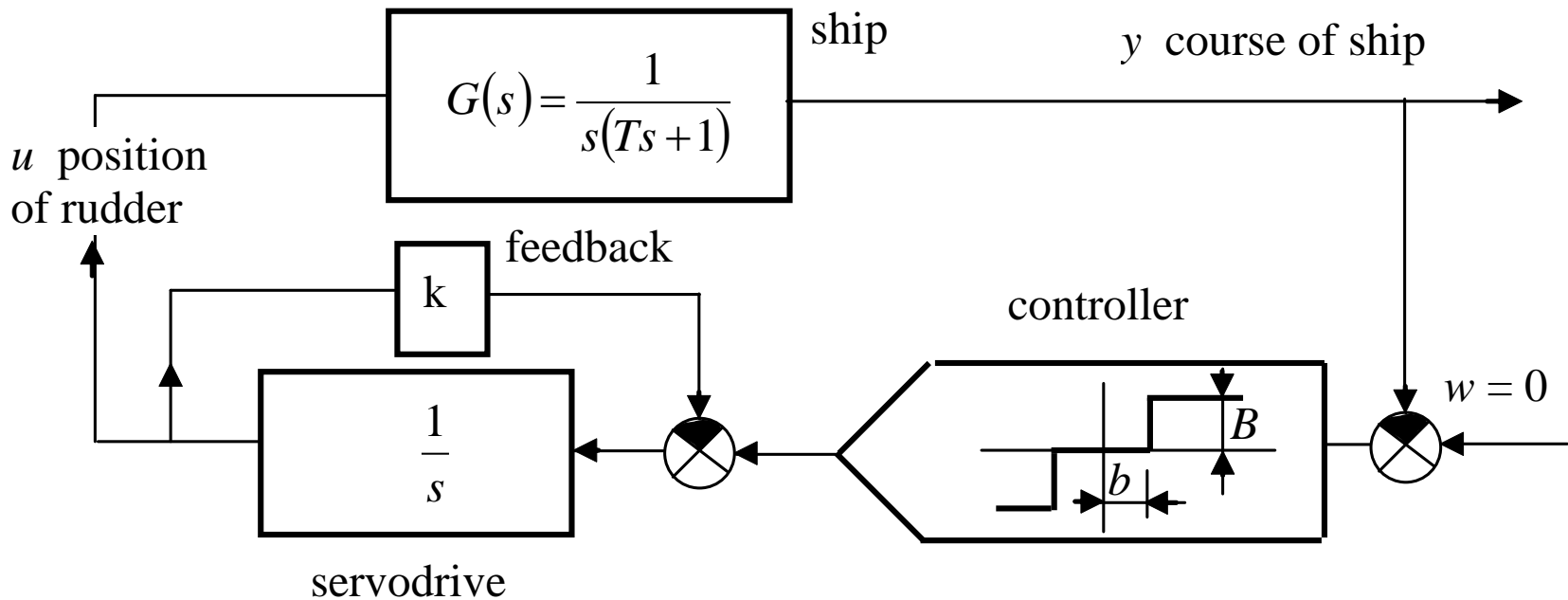
$$G_N(A) = -\frac{1}{G_L(j\omega)} \rightarrow G_N(A) = \frac{4B}{\pi A}$$

$$-\frac{1}{G_L(j\omega)} = -\frac{1}{k} j\omega(T_1 j\omega + 1)(T_2 j\omega + 1)$$



$$\omega = 0,31; \quad A = 1,2$$

**Example:** Course of ship is controlled using three-value controller. Scheme of controller circuit in figure. Time constant of the ship as controlled system is  $T = 100$  s and gain  $k = 10$ . Determine when the autooscillations do not emerge.



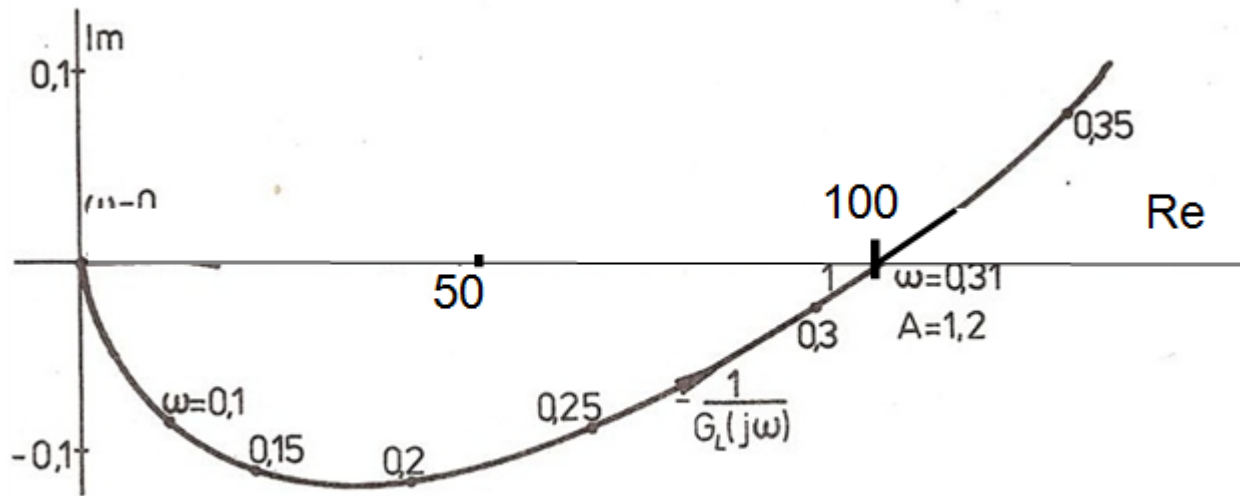


**Solution:** Linear member

Condition for autooscillation emergence

$$G(s) = \frac{1}{s(Ts + 1)(s + k)}$$

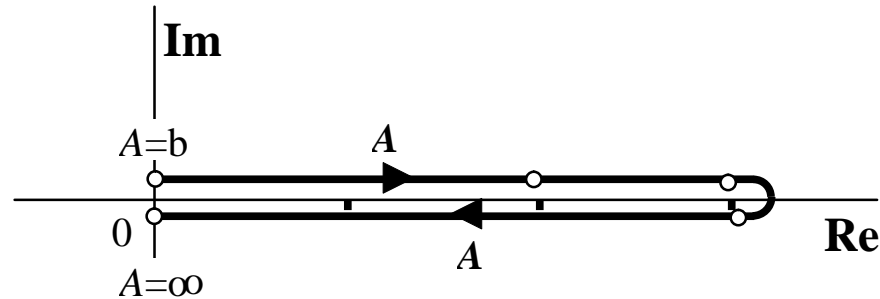
$$G_N(A) = -\frac{1}{G_L(j\omega)}$$



Equivalent transfer of nonlinear member and it's amplitude characteristics.

$$G_N(A) = \frac{4B}{\pi A} \sqrt{1 - \frac{b^2}{A^2}}$$

Value A for which is maximum of characteristic.



For derivative use these formulas:

|                   |                       |                     |                            |
|-------------------|-----------------------|---------------------|----------------------------|
| $y = uv$          | $y' = u'v + uv'$      | $y = \frac{1}{x^2}$ | $y' = -\frac{2}{x^3}$      |
| $y = \frac{1}{x}$ | $y' = -\frac{1}{x^2}$ | $y = \sqrt{x}$      | $y' = \frac{1}{2\sqrt{x}}$ |

$$\frac{dG_N(A)}{dA} = 0$$

Derivative  $\frac{dG_N(A)}{dA} = 0$

$$\left( \frac{4B}{\pi A} \sqrt{1 - \frac{b^2}{A^2}} \right)' = -\frac{4B}{\pi A^2} \sqrt{1 - \frac{b^2}{A^2}} + \frac{4B}{\pi A} \frac{1}{2\sqrt{1 - \frac{b^2}{A^2}}} \frac{2b^2}{A^3} = 0 \quad -\sqrt{1 - \frac{b^2}{A^2}} + \frac{b^2}{A^2} \frac{1}{\sqrt{1 - \frac{b^2}{A^2}}} = 0$$

$$-\left(1 - \frac{b^2}{A^2}\right) + \frac{b^2}{A^2} = 0 \quad \Rightarrow \quad -1 + 2\frac{b^2}{A^2} = 0 \quad \Rightarrow \quad \frac{b^2}{A^2} = \frac{1}{2}$$

$$\frac{b}{A} = \frac{1}{\sqrt{2}} \quad \Rightarrow \quad A = b\sqrt{2}$$

So the characteristics will not intersect (autooscillations will not emerge).

$$G_N(A) = \frac{4B}{\pi A} \sqrt{1 - \frac{b^2}{A^2}} = \frac{4B}{\pi b\sqrt{2}} \sqrt{1 - \frac{b^2}{b^2 \cdot 2}} < 100$$